

# **BUH615**

## HIGH VOLTAGE FASTSWITCHING NPN POWER TRANSISTOR

- SGS-THOMSON PREFERRED SALESTYPE
- HIGH VOLTAGE CAPABILITY
- U.L. RECOGNISED ISOWATT218 PACKAGE (U.L. FILE # E81734 (N))

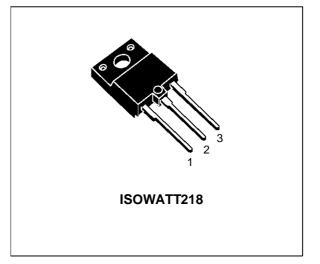
## **APPLICATIONS:**

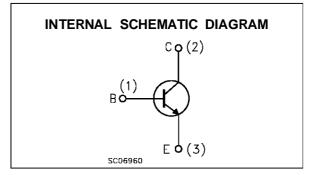
 HORIZONTAL DEFLECTION FOR COLOUR TVS AND MONITORS

### DESCRIPTION

The BUH615 is manufactured using Multiepitaxial Mesa technology for cost-effective high performance.

The BUH series is designed for use in horizontal deflection circuits in televisions and monitors.





### **ABSOLUTE MAXIMUM RATINGS**

Symbol	Parameter	Value	Unit
V <sub>CBO</sub>	Collector-Base Voltage $(I_E = 0)$	1500	V
Vceo	Collector-Emitter Voltage $(I_B = 0)$	700	V
$V_{EBO}$	Emitter-Base Voltage $(I_C = 0)$	10	V
lc	Collector Current	8	A
I <sub>CM</sub>	Collector Peak Current (t <sub>p</sub> < 5 ms)	15	A
Ι <sub>Β</sub>	Base Current	5	A
I <sub>BM</sub>	Base Peak Current (t <sub>p</sub> < 5 ms)	8	A
P <sub>tot</sub>	Total Dissipation at $T_c = 25$ °C	54	W
T <sub>stg</sub>	Storage Temperature	-65 to 150	°C
Tj	Max. Operating Junction Temperature	150	°C

## THERMAL DATA

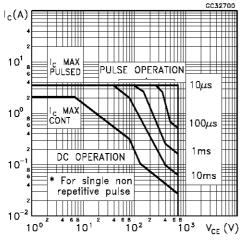
R <sub>thj-case</sub> Thermal Resistance Junction-case	Max 2	.3 °C/W
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## **ELECTRICAL CHARACTERISTICS** ( $T_{case} = 25 \, {}^{\circ}C$ unless otherwise specified)

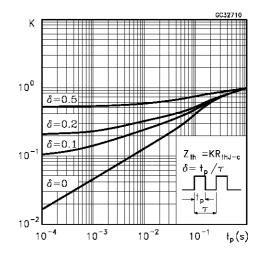
Symbol	Parameter	Test Conditions	Min. Typ. Max.			Unit	
I <sub>CES</sub>	Collector Cut-off Current ( $V_{BE} = 0$ )	$V_{CE} = 1500 V$ $V_{CE} = 1500 V$ $T_j = 125 °C$			1 2	mA mA	
I <sub>EBO</sub>	Emitter Cut-off Current $(I_C = 0)$	V <sub>EB</sub> = 5 V			100	μA	
V <sub>CEO(sus)</sub>	Collector-Emitter Sustaining Voltage	I <sub>C</sub> = 100 mA	700			V	
$V_{\text{EBO}}$	Emitter-Base Voltage (I <sub>C</sub> = 0)	I <sub>E</sub> = 10 mA	10			V	
$V_{CE(sat)}*$	Collector-Emitter Saturation Voltage	$I_{\rm C} = 6 \ {\rm A}  I_{\rm B} = 1.5 \ {\rm A}$			1.5	V	
V <sub>BE(sat)</sub> *	Base-Emitter Saturation Voltage	$I_{\rm C} = 6 \ {\rm A}  I_{\rm B} = 1.5 \ {\rm A}$			1.3	V	
h <sub>FE</sub> *	DC Current Gain	$I_C = 5 A$ $V_{CE} = 5 V$	5				
t <sub>s</sub> t <sub>f</sub>	RESISTIVE LOAD Storage Time Fall Time	$V_{CC} = 400 V$ $I_C = 5 A$ $I_{B1} = 1.25 A$ $I_{B2} = 2.5 A$		2.7 190	3.9 280	μs ns	
t <sub>s</sub> t <sub>f</sub>	INDUCTIVE LOAD Storage Time Fall Time	$I_{C} = 5 A \qquad f = 15625 \text{ Hz} \\ I_{B1} = 1.25 A \qquad I_{B2} = -2.5 A \\ V_{ceflyback} = 1050 \sin\left(\frac{\pi}{10} \ 10^{6}\right) t  V$		2.3 370		μs ns	
t <sub>s</sub> t <sub>f</sub>	INDUCTIVE LOAD Storage Time Fall Time	$ \begin{array}{l} I_{C} = 5 \ A & f = 31250 \ Hz \\ I_{B1} = 1.25 \ A & I_{B2} = -2.5 \ A \\ V_{ceflyback} = 1200 \ sin\left(\frac{\pi}{5} \ 10^{6}\right) t \ V \end{array} $		2.3 210		μs ns	

\* Pulsed: Pulse duration = 300 μs, duty cycle 1.5 %

## Safe Operating Area

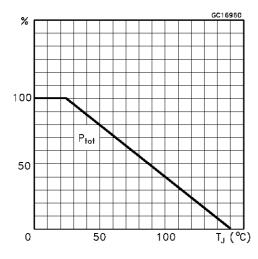


Thermal Impedance

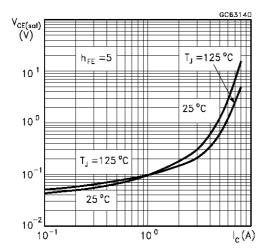




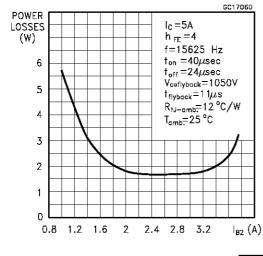
## **Derating Curve**



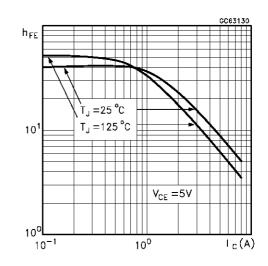
Collector Emitter Saturation Voltage



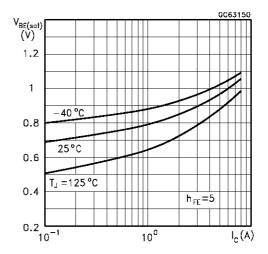
## Power Losses at 16KHz



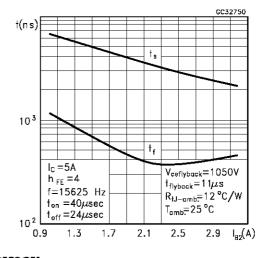
DC Current Gain



## Base Emitter Saturation Voltage

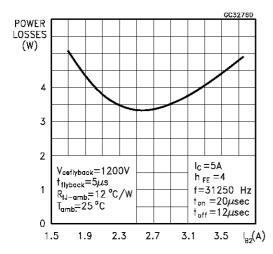


Switching Time Inductive Load at 16KHz (see figure 2)

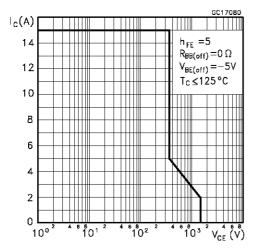




Power Losses at 32KHz



**Reverse Biased SOA** 

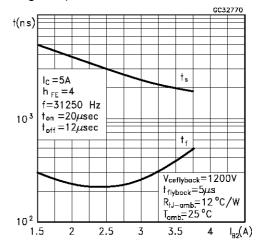


## **BASE DRIVE INFORMATION**

In order to saturate the power switch and reduce conduction losses, adequate direct base current  $I_{B1}$  has to be provided for the lowest gain  $h_{FE}$  at 100 °C (line scan phase). On the other hand, negative base current  $I_{B2}$  must be provided to turn off the power transistor (retrace phase).

Most of the dissipation, in the deflection application, occurs at switch-off. Therefore it is essential to determine the value of  $I_{B2}$  which minimizes power losses, fall time  $t_f$  and, consequently,  $T_j$ . A new set of curves have been defined to give total power losses,  $t_s$  and  $t_f$  as a function of  $I_{B2}$  at both 16 KHz and 32 KHz scanning frequencies for choosing the optimum negative drive. The test circuit is illustrated in

Switching Time Inductive Load at 32KHz (see figure 2)





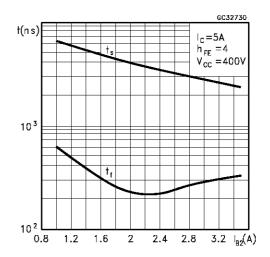


figure 1.

Inductance  $L_1$  serves to control the slope of the negative base current  $I_{B2}$  to recombine the excess carrier in the collector when base current is still present, this would avoid any tailing phenomenon in the collector current.

The values of L and C are calculated from the following equations:

$$\frac{1}{2}L(I_{C})^{2} = \frac{1}{2}C(V_{CEfly})^{2} \qquad \omega = 2\pi f = \frac{1}{\sqrt{LC}}$$

Where  $I_{C}$ = operating collector current,  $V_{CEfly}$ = flyback voltage, f= frequency of oscillation during retrace.



Figure 1: Inductive Load Switching Test Circuits.

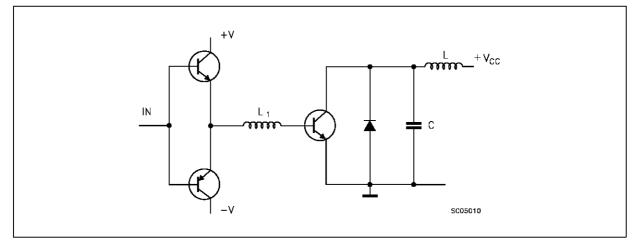
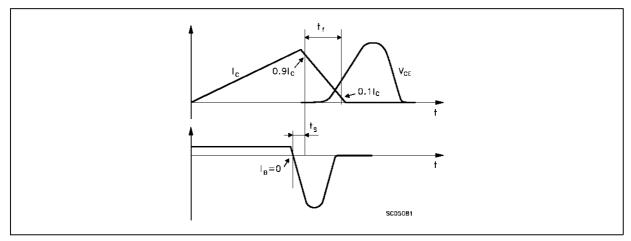


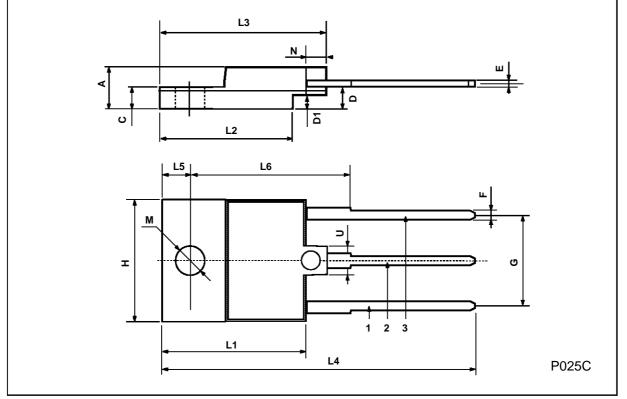
Figure 2: Switching Waveforms in a Deflection Circuit





DIM.		mm			inch	
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.
А	5.35		5.65	0.210		0.222
С	3.3		3.8	0.130		0.149
D	2.9		3.1	0.114		0.122
D1	1.88		2.08	0.074		0.081
Е	0.45		1	0.017		0.039
F	1.05		1.25	0.041		0.049
G	10.8		11.2	0.425		0.441
Н	15.8		16.2	0.622		0.637
L1	20.8		21.2	0.818		0.834
L2	19.1		19.9	0.752		0.783
L3	22.8		23.6	0.897		0.929
L4	40.5		42.5	1.594		1.673
L5	4.85		5.25	0.190		0.206
L6	20.25		20.75	0.797		0.817
М	3.5		3.7	0.137		0.145
Ν	2.1		2.3	0.082		0.090





6/7

**BUH615** 

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